feature	Top	bottom	depth
78	57.638	57.068	.570
60	57.688	57.148	.540
58	57.704	57.102	.602
16	57.893	57.313	.580
99	58.083	57.512	.571
134	58.277	57.689	.588

fenceline

AREA I

UNITS TRANSITIONAL BETWEEN TERRACES

Terraces 3-4	~~482~~	562	236
	~~441~~	521	196
	~~319~~	481	155
	~~276~~	440	114
	~~23~~	399	73
	~~19~~	359	33
	~~5~~	318	
	~~34~~	277	
Terraces 2-3	388		
	389		
	309		
	268		
	228		
	187		
	146		
	147		
	106		
	66		
	26		
	806		
	807		
	766		
	767		
	726		
	727		

Terracus 1-2

217
176
136
95
96
97
98
100
60
20
21
802
803
763

TERRACE I	TERRACE 2
12 - 19	22 - 25
53 - 59	61 - 65
94	101 - 105
132 - 135	137 - 145
173 - 175	177 - 186
214 - 216	218 - 227
256 - 257	259 - 267
792 - 800	298 - 308
751 - 762	340 - 349
710 - 721	380 - 387
671 - 680	682 - 686
948 - 950	723 - 725
	764 - 765
	804 - 805
	929
	956

TERRACE 4	
34 - 36	400 - 405
74 - 77	441 - 446
115 - 118	482 - 487
156 - 159	523 - 528
197 - 200	563 - 569
237 - 241	607
278 - 282	648
319 - 323	
360 - 364	

EVERYTHING ELSE IS TERRACE

3

VI-5 datum for Figure VI-3
S216/E233 - 58.510

VI II datum for well & Figure VI-7-
FROM: I beam - 60.452
FROM: S216 E232.63 - 58.052

VI-65 datum used for cellar
K6A6001 MAIN DATUM: S207 E287.1 - 58.267

VI-97 soil description of F.7004
F7004 Z11, Z12, Z15 - 10YR 3/2 very dark grayish brown.

F7004 Z13, Z14 - 10YR 3/3 dark brown silty loam.

VI-98 F7137 or 7135
is F.7137.

VI-76 POST MOLDS OF FEATURES 6002 & 6021

6002 — 57.368

22cm N-S, 22cm E-W, 72cm deep.

6021 —

24cm N-S, 22cm E-W, 69cm deep 57.001

VI-97- DIMENSIONS OF MOLDS OF 7014, 7015, 7018, 7021, 7028, 7050.

7014 —

35cm N-S, 38cm E-W, 37cm deep 59.309

7015 —

28cm N-S, 30cm E-W, 24.5cm deep 59.264

7018 —

17cm N-S, 17cm E-W, 32cm deep. 59.549

7021 —

19cm N-S, 17cm E-W, 23cm deep 59.349

7028 —

24.5cm N-S, 24.5cm E-W, 39.5cm deep 59.205

7050 —

20cm N-S, 20cm E-W, 65cm deep 59.207

References to boards in K6A6001 - cellar

(6/27/85) Chuck Norville pg. 138 - "The floor boards in Units 37, 47, 57, and 36 were oriented N-S which leads to the conclusion that those in Unit 49 (and others) are collapse debris due to their random orientation."

pg. 138 - "The board remnants appear on all three walls that have been exposed so far, though not consistantly or in the expected locations close to the walls of the cellar. They are least well exposed along the west wall; best along the north."

UNITS

36 Level H - Wood flooring, seen also in units 37, 47, + 57.

37 Level D - Board at 74cm.

Level F - Small wood fragments scattered through out level.

Level G Boards at 128cm.

38 Level F - Lots of wood + charcoal

Level G - Badly deteriorated piece of lumber crossing unit diagonally.

Level H - Pieces of lumber with haphazard distribution - no two pieces side by side or in any pattern.

Level I - Some decayed wood (planks)

39 Level H - Wood stains present.

40 Level D - Wood plank w/ rotted portions - stain left by wood plank.

47 Level D - One wood stain.

Level E - Boards associated w/ flooring planks, extended into unit from Unit 37.

(OVER)

UNITS:

48 Level F - Very decayed wood pieces.
Level G - Large wood planks running haphazardly through unit.

49 Level D - Some wood in this level, could not tell if cut board or rot, only 5 cm wide, very deteriorated.
Level E - Lots of very deteriorated wood fragments found near floor of unit.

50 Level E - Bottom of level revealed a wood plank running north-south approximately 30 cm from east wall of cellar.

57 Level E - Board mold in north profile. "Humic stain runs through unit & shows in west profile as possible lining of cellar." Wood planks extend from Level E-F.

58 Level E - Contains wood, may be organic debris or erosional surface.
Level G - Near south wall of unit are several decayed wood pieces.

VI-68 MEASUREMENTS OF WOOD FROM WELL

5/22 K101002061

FIRST PLANK 13.85m below I beam

95cm long, 10cm wide, 2cm thick

5/22 K101002062

PARTIAL BOARD REMOVED

INTACT WIDTH - 12.5cm WIDE, 1.5cm THICK

SECOND, WHOLE, BOARD

2.11m long. TWO MORE BOARDS REMOVED —

2.11m LONG.

5/23 K101002063

PIECE OF WOOD 14.13m below I beam.

27cm x 8cm x 2cm. Small stake in front of boards - 2½cm wide.

5/23 K101002064

WOOD PLANK PULLED OUT AT 14.00m from I beam.

5/28 K101002067

SIX SMALLER PLANKS REMOVED AT 14.48m below I beam

6/5 K101002076

MEASUREMENT ON TOP OF PLANKS LEFT STANDING IN WELL 14.71m below top of I beam OR 12.31m below main datum at ground level.

MEASUREMENTS OF PLANKS REMOVED FROM WELL: 185cm length x 11cm x 1.5cm,

185cm x 11cm x 1.5cm & 185cm x 13.5cm x 2cm.

6/6

Planks out of well

185 cm length x 11 cm x 1.5 cm
185 cm x 11 cm x 1.5 cm
185 cm x 13.5 cm x 2 cm

Square nail holes in each plank at each end w/ possible exception of one end of largest plank. ~~there~~

Shaded area at the left of the picture shows the discolored portion that was present on one side of each plank, where they perhaps overlapped ~~overlapped~~ each other from between 1 cm and ~~2 cm~~ a little less than 2 cm.

Felt like I could see an impression about barrel stave width at each nail hole - like rings of wood had been around inside and nailed in place.

~~Nail holes~~

✓ VI-5 get datum for Fig VI-3

✓ VI-11 " " for well & Fig VI-7

✓ VI-12 same as

✓ VI-19 Table VI-1 & sentence do not agree check data

~~WILL TAKE TIME~~

VI-23 ~~[illegible]~~ own artif. patterns for all POSTHOLES in area I

D ✓

Page VI-5 Fig VI-3 find correct coordinates for profile & try to find a good N-S profile instead

✓ ✓

VI-41 redo level designations ~~arabic & letters not roman numerals~~ — ~~make it similar to other areas~~ So Figs VI-21 & VI-22 agree

✓ ✓

VI-43 find Hurry artifact lists for Area 4 — Plot on Fig. VI-23 map plot our prehistoric on map

✓ ✓

[redacted]

~~VI-53 redo level designations to arabic & letters~~

VI-62 Fig. VI-32 find as many N-S profiles as possible - string them together w/ gaps if necessary & reverse any so that they are all viewed from same direction.

✓ VI-65 Fig. VI-34 datum used in cellar
USE ✓

VI-68 STEVE find all references in notes to boards - on bottom, in fill and along wall

✓ Also measurements of wood from well

VI-76 ✓ Check for molds on features 6002 & 6021

VI-96 ✓ List dimensions of molds of #7014 ✓7021, ✓7015 ✓7018 ✓7028 ✓7050

VI-97 ✓ Soil description of #7004

✓ VI-98 F 7157 or 7155 check -

✓ VI-99 ~~art pattern of F~~
List all artifacts for units near road in area VI-B

✓ VI-103 ~~find~~ list all artifacts in VI-d

ASSUMING TERR I is original ground surface

~~[illegible]~~ cu. meters removed from terracing

~~Terr~~	area	amt cut (difference in depth between ~~from terrace~~ terr 1 depth)	Cub meters removed
Terr 1	.155	Ø	Ø
Terr 2	128	.126 ~~[illegible]~~/2=	8.06
Terr 3	173	.139 ~~[illegible]~~/2 =	12.02
Terr 4	123 *	.024 ~~[illegible]~~/2 =	2.08
			22.156

* at least as large as terrace III

Cellar 7.5 X 5.25 X 1.85 = 72.84 — total cellar

Cellar 7.5 X 5.25 X .75 = 29.53 — Dark layers at bottom of cellar

Red fill TPQ 1840
MCD 1793.55

Organic fill TPQ 1840
MCD 1789.18

Floor TPQ 1840
MCD 1789.85

ASSUMING AREA I

WAS ORIGINAL GROUND SURFACE
& Terrace I has been cut

~~Area~~	area	amt cut above area I	cubic meters removed
Terr 1	155	(.431-.429)/2 = .001	.155
Terr 2	128	(.431-.303)/2 = .064	8.192
Terr 3	173	(.431-.290)/2 = .071	12.283
Terr 4	173*	(.431-.405)/2 = .013	2.249
			22.879

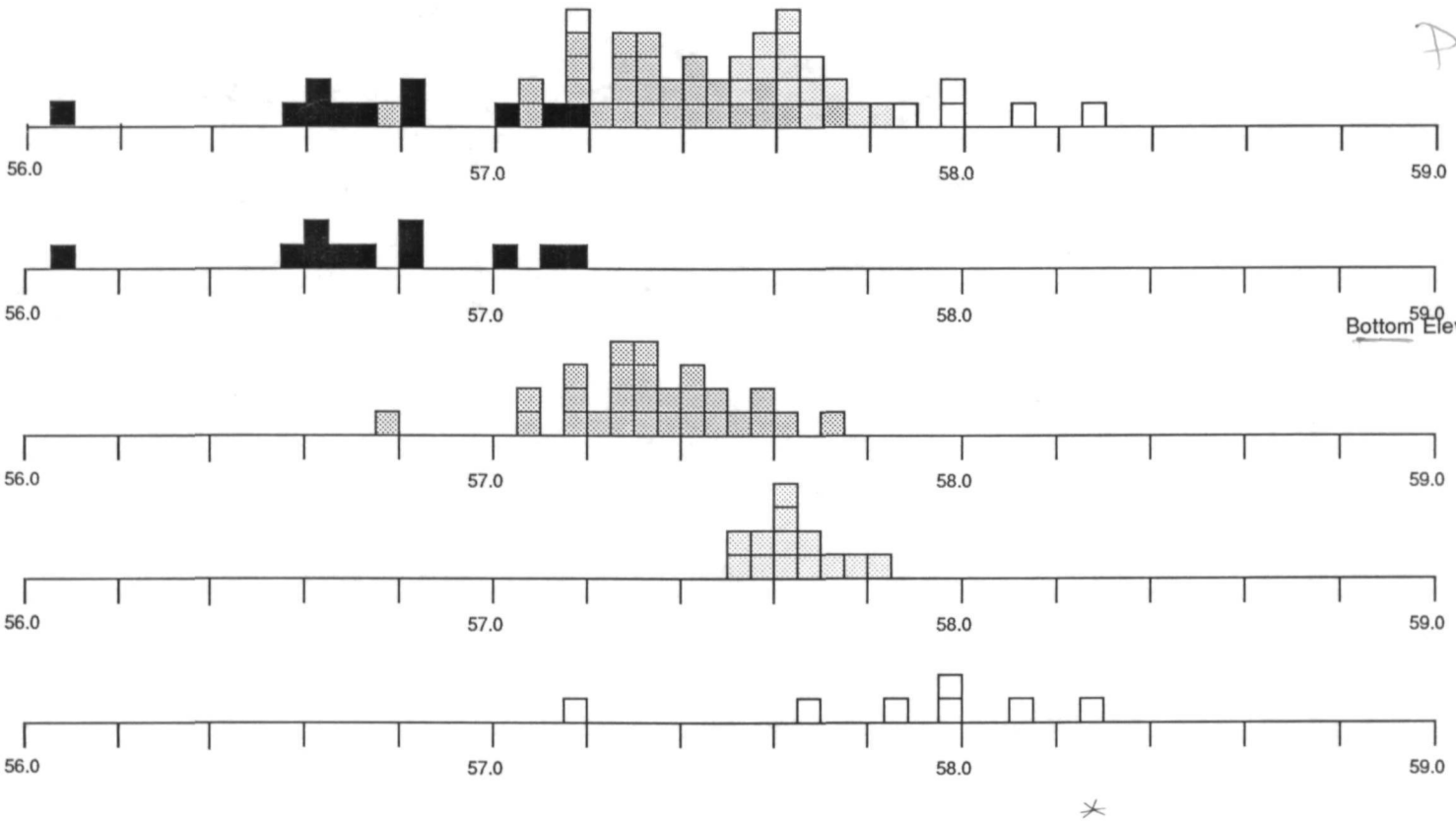
STRUCTURAL
POST HOLES ONLY

TERRACE		$\bar{X}$	Range		σ	standard error ~~Z SCORE~~	N
1	TOP	58.294	58.126-58.562	.436	.163	.062	7
1	bottom	57.865	57.152 - 58.292	1.14	.369	.139	7
1	depth	.429	.210 - .974	.764	.268	.101	7
2	top	57.95	57.854 - 58.062	.208	.067	.019	13
2	bottom	57.648	57.514 - 57.842	.328	.095	.026	13
2	depth	.303	.205 - .470	.265	.082	.023	13
3	top	57.625 57.632	57.381 - 57.832	.451	.121 .118	.022 ok	29 28
3	bottom	57.351 57.339	56.769 - 57.702	.933	.200 .193	.037 .036	29 28
3	depth	.291 .292	.080 - .975	.895	.168 .171	.031 .032	29 28
4	top	57.118 ~~57.468~~ ~~57.118~~	56.818 - 57.290 ~~57.290~~	.472 ~~1.141~~ ~~.472~~	.147 ~~.417~~ ~~.147~~	.046 ~~.098~~ ~~.046~~	~~18~~ 10
4	bottom	56.713 ~~57.119~~	56.083 - 57.177 ~~57.118~~	1.094 ~~1.635~~	.294 ~~.516~~	.093 ~~.122~~	~~18~~ 10
4	depth	~~.349~~ ~~.405~~ .405	.040 - .925	.885	~~.220~~ ~~.284~~ .284	~~.052~~ ~~.040~~ .090	~~18~~ 10
all	top	57.691 57.695	56.818 - 58.562	1.744	.363 .365	.047 .048	59 58
all ~~bottom~~	bottom	57.369 57.364	56.083 - 58.292	2.209	.412 .414	.054	59 58
all	depth	.329 .331	.04 - .975	.935	.195 .196	.025 .026 ok	59 58
structural Pholes subsumed by 19, 25, 28, 96 & 231 & 117 28-117	TOP						
	bottom	57.450 ~~57.345~~	57.170 - 57.693 ~~57.631~~	.523 ~~.461~~	.166 ~~.142~~	.027 ~~.026~~	38
	~~depth~~	~~.285~~	~~.184-.408~~	~~.224~~	~~.065~~	~~.011~~	~~38~~

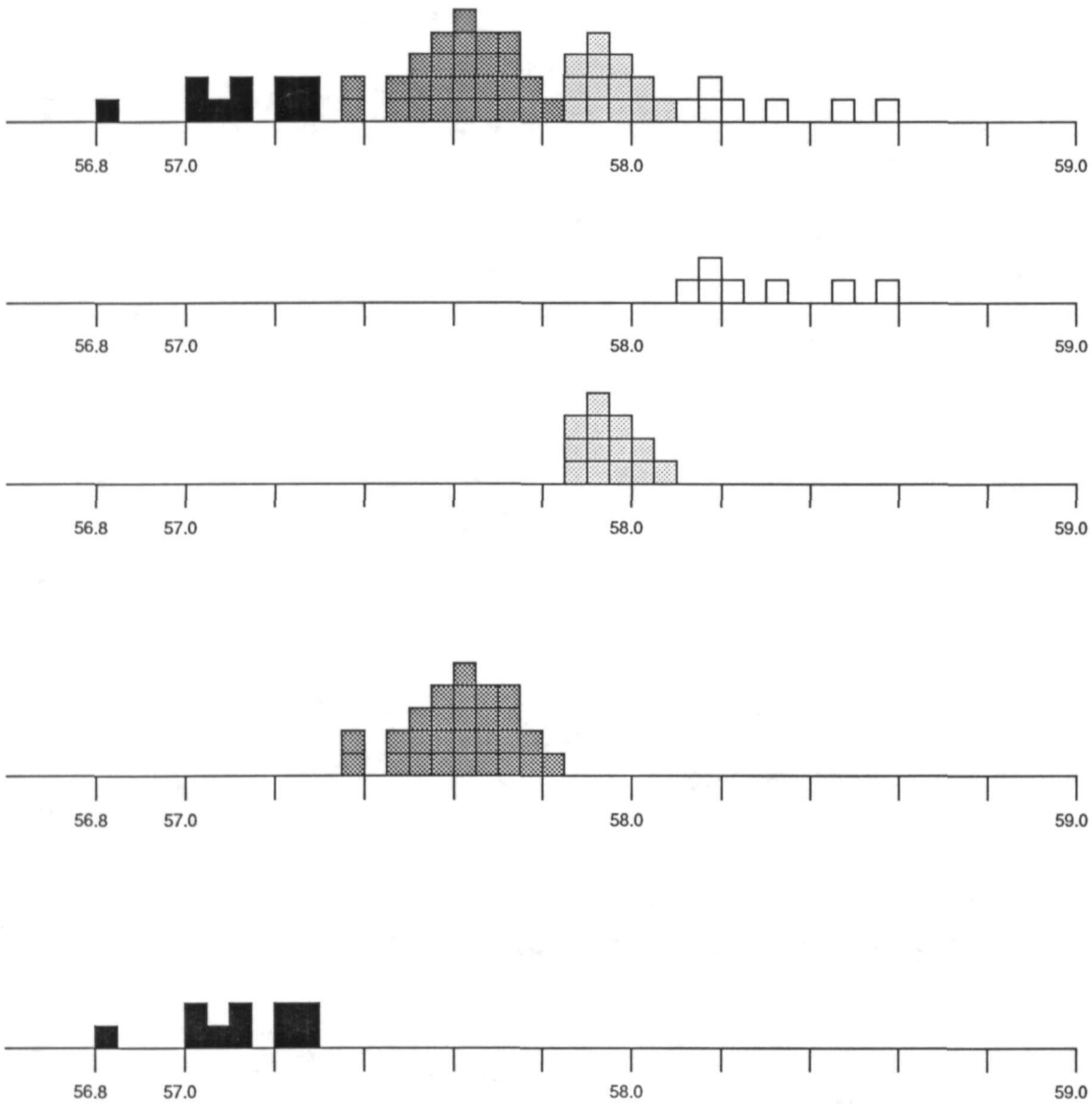
~~AREA VI A~~

	$\bar{X}$	Range		σ	standard error	n
AREA VIa						
TOP	57.868	57.542-58.368	.826	.283	.100	8
BOTTOM	57.285	57.071-57.615	.544	.205	.072	8
DEPTH	.582	.380-.900	.520	.180	.064	8
AREA V						
TOP	59.033	58.976-59.086	.110	.035	.012	8
BOTTOM	58.602	58.520-58.674	.154	.051	.018	8
DEPTH	.431	.350-.490	.140	.055	.019	8
FENCELINE AREA I						
TOP	57.877	57.638-58.277	.639	.255	.104	6
BOTTOM	57.305	57.068-57.689	.621	.250	.102	6
DEPTH	.575	.540-.602	.062	.021	.009	6

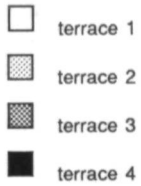
STRUCTURAL POSTHOLES BOTTOM ELEV



STRUCTURAL
POST HOLES
TOP ELEV.

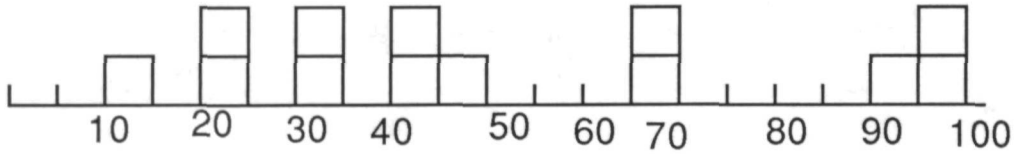


Top Elevations of Postholes

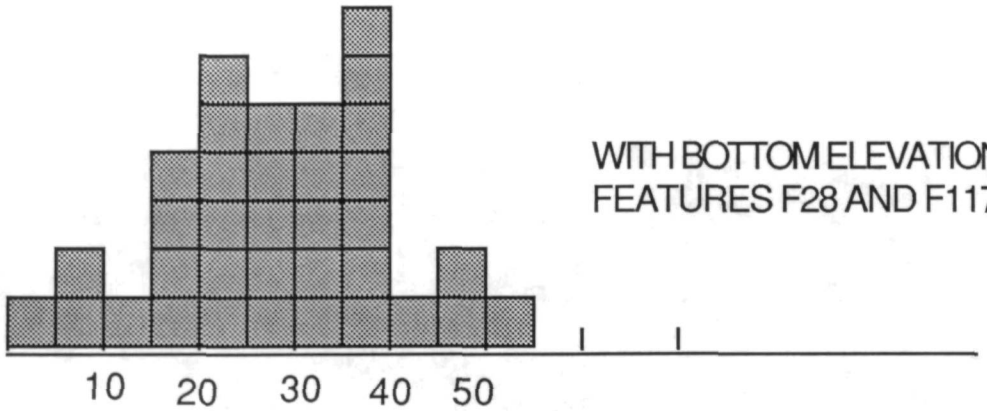


STRUCTURAL POSTHOLE DEPTHS IN CENTIMETERS

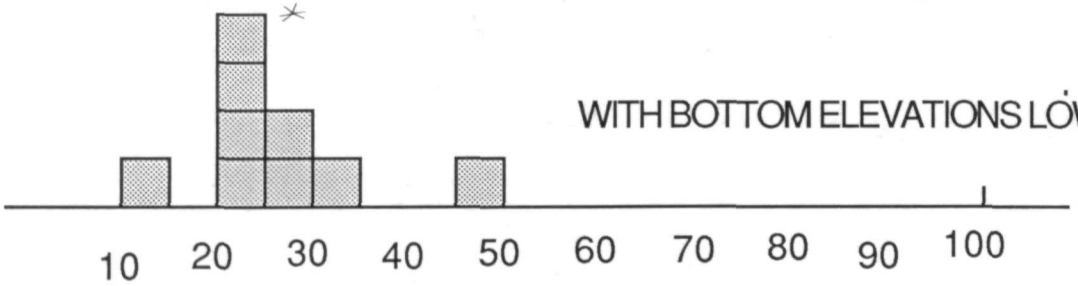
WITH BOTTOM ELEVATIONS GREATER THAN F 117



WITH BOTTOM ELEVATIONS BETWEEN FEATURES F28 AND F117

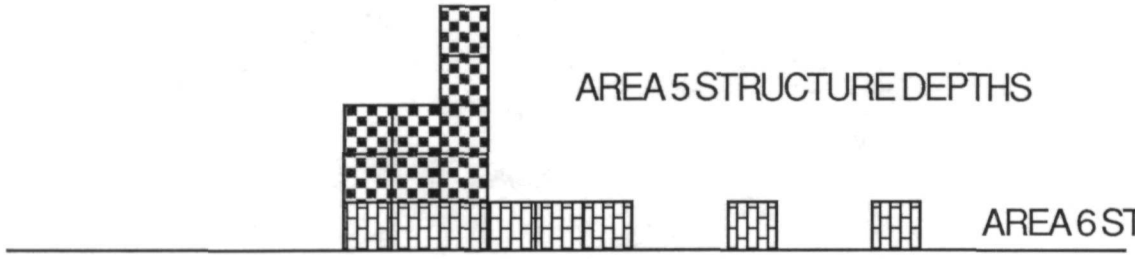


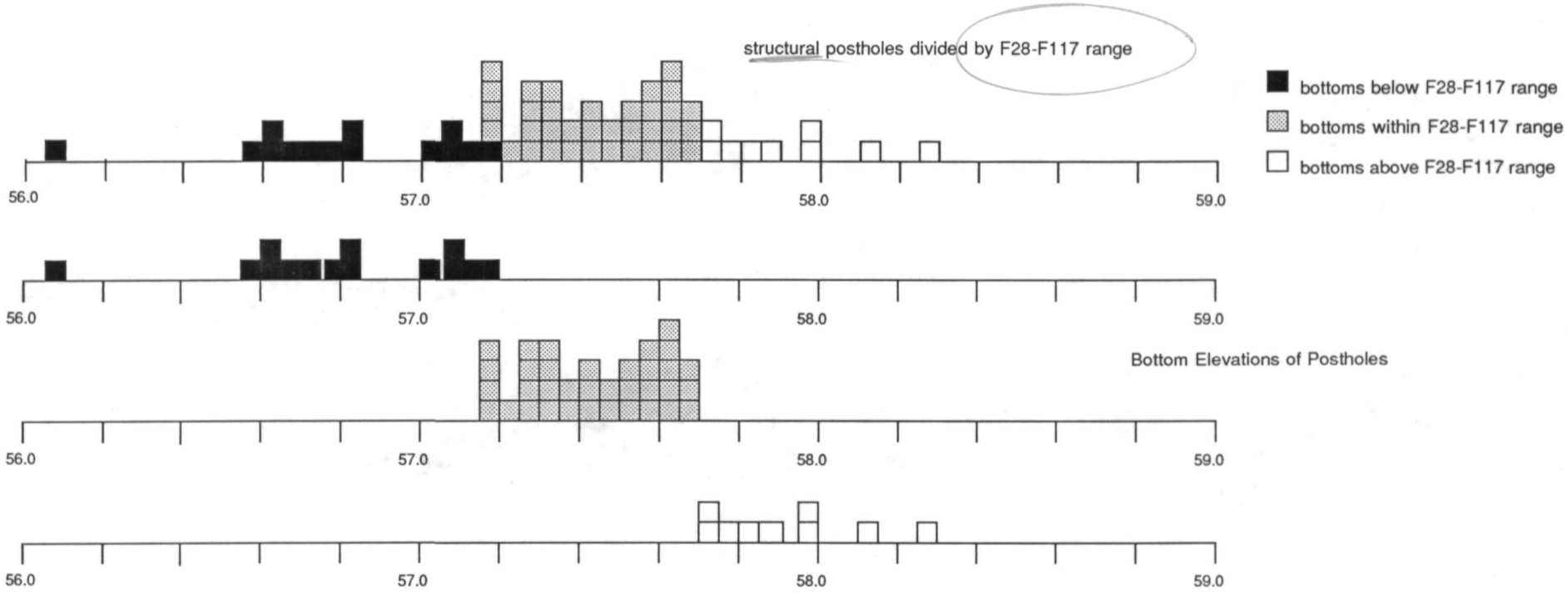
WITH BOTTOM ELEVATIONS LOWER THAN F 28



AREA 5 STRUCTURE DEPTHS

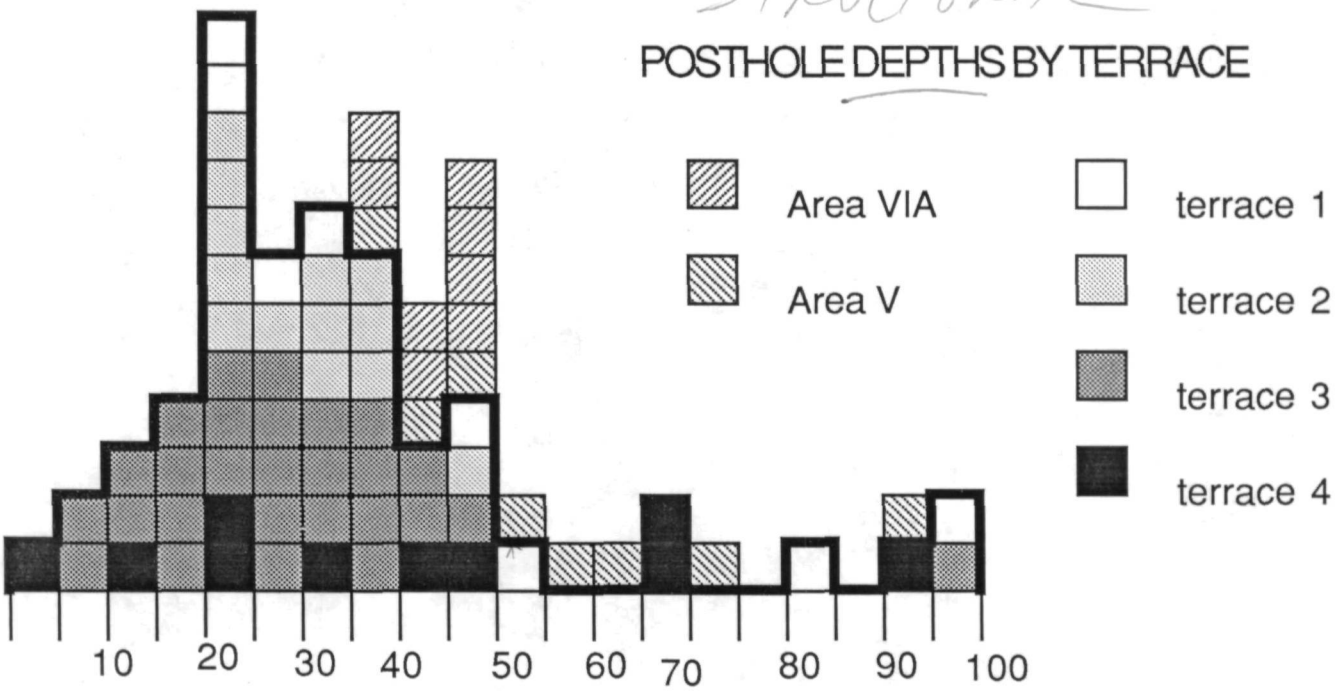
AREA 6 STRUCTURE DEPTHS

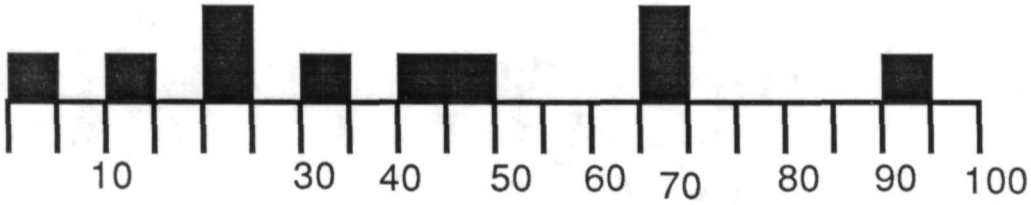


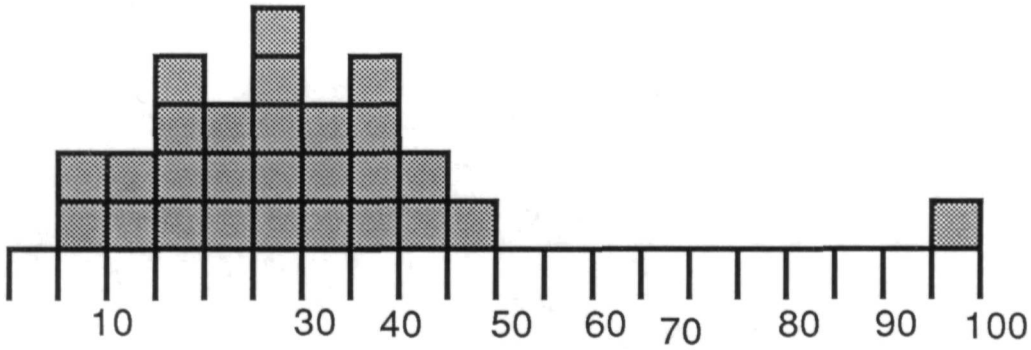

structural postholes divided by F28-F117 range
bottoms below F28-F117 range
bottoms within F28-F117 range
bottoms above F28-F117 range
56.0
57.0
58.0
59.0
Bottom Elevations of Postholes

STRUCTURAL

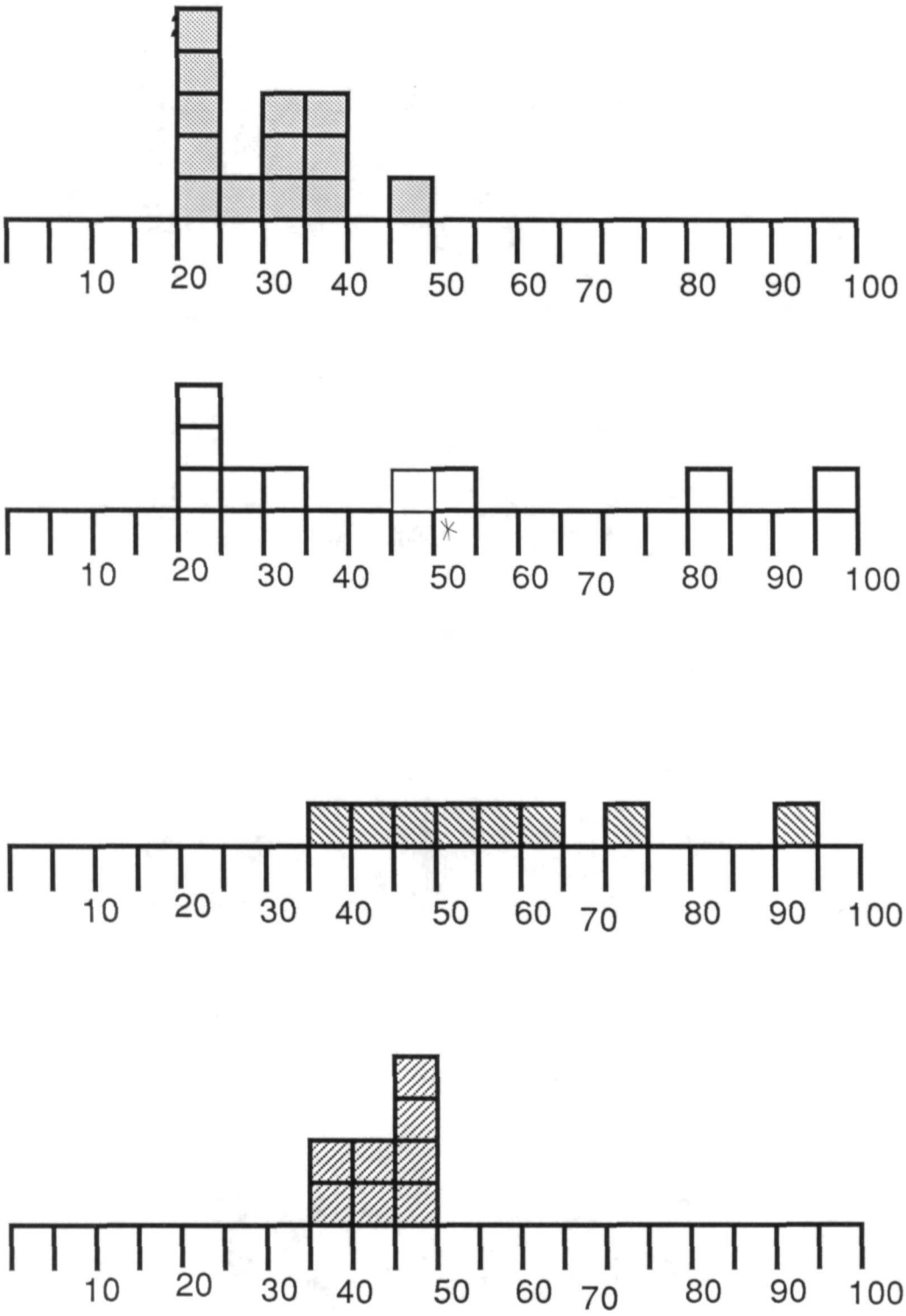
POSTHOLE DEPTHS BY TERRACE







POSTHOLE DEPTHS BY TERRACE



STRUCTURAL POST HOLES

#	bottom	top	depth
113	56.083	57.008	.925
179	56.596	57.290	.694
206	56.605	57.065	.460
104	56.622	57.272	.650
46	56.672	57.109	.437
48	56.718	56.818	.100
111	56.769	57.744	.975
239	56.805	57.025	.220
207	56.807	57.132	.325
125	57.047	57.247	.200
18	57.062	57.397	.335
29	57.085	57.499	.414
232	57.152	58.126	.974
28	57.170	57.531	.361
249	57.177	57.217	.040
204	57.189	57.685	.496
30	57.193	57.552	.359
72	57.233	57.593	.360
268	57.261	57.381	.120
231	57.269	57.677	.408
26	57.272	57.492	.220
244	57.296	57.636	.340
247	57.306	57.616	.310
267	57.311	57.531	.220
164	57.326	57.591	.265
90	57.345	57.625	.280
92	57.369	57.642	.273
94	57.383	57.748	.365
19	57.400	57.584	.184
162	57.431	57.511	.080
221	57.440	57.800	.360
25	57.448	57.728	.280
266	57.451	57.611	.160
73	57.491	57.741	.250
222	57.511	57.682	.171
3	57.514	57.854	.340
62	57.524	57.994	.470
215	57.548	57.698	.150
241	57.552	57.872	.320
83	57.572	57.932	.360

SORTED BY BOTTOM ELEV.

June 1

22	57.582	57.774	.192
45	57.588	57.788	.200
20	57.618	57.698	.160
95	57.631	57.981	.350
129	57.632	57.962	.330
224	57.646	58.044	.398
96	57.649	57.881	.232
136	57.682	57.912	.230
60	57.688	57.448	.240
242	57.692	57.912	.220
117	57.693	58.230	.537
160	57.702	57.832	.130
220	57.718	57.923	.205
208	57.764	58.027	.263
50	57.842	58.062	.220
7	57.857	58.312	.455
14	57.952	58.192	.240
237	57.962	58.172	.210
182	58.147	58.467	.320
218	58.292	58.562	.270
6023	•	•	•
6031	•	•	•
6035	•	•	•
6021	•	•	•
6012	•	•	•
6002	•	•	•
6020	•	•	•
6015	•	•	•

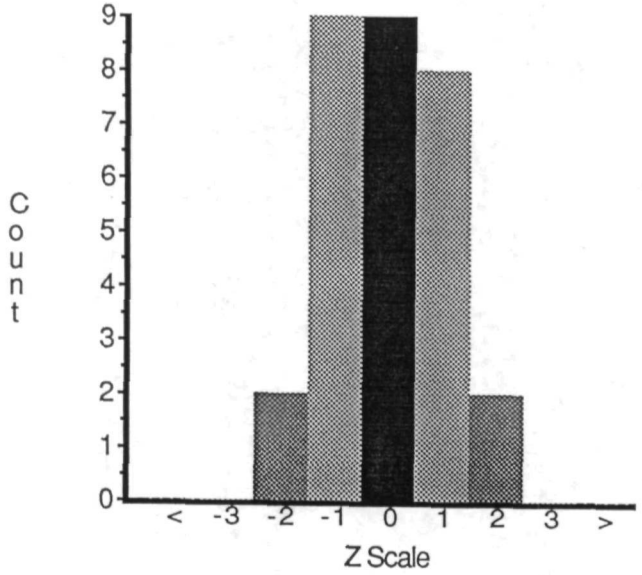
Sensitive

Stat. 28 - 117

BOTTOM ELEVATION

Mean:	Std. Dev.:	Std. Error:	Variance:	Coef. Var.:	Count:
57.45	.166	.027	.028	.29	38
Minimum:	Maximum:	Range:	Sum:	Sum Squared:	# Missing:
57.17	57.693	.523	2183.083	125418.167	0
Median:	Mode:	Kurtosis:	Skewness:		
57.45	•	-1.256	-.126		

Z Score of BOTTOM ELEVATION

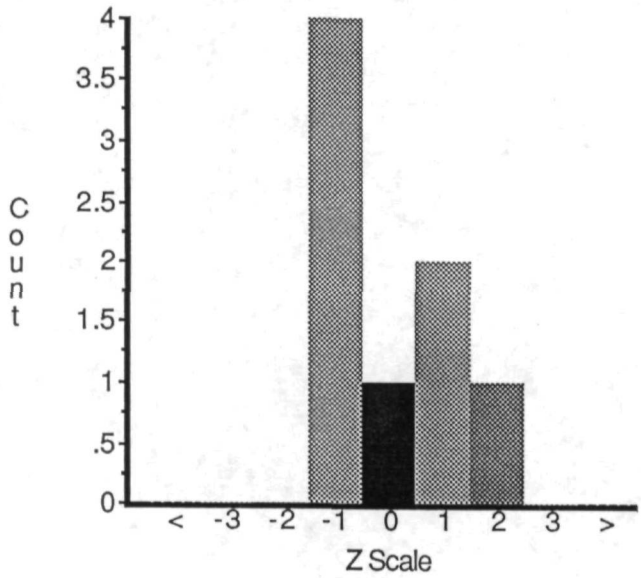


range of 19, 25, 28, 95, 231

BOTTOM ELEVATION

Mean:	Std. Dev.:	Std. Error:	Variance:	Coef. Var.:	Count:
57.395	.142	.026	.02	.248	30
Minimum:	Maximum:	Range:	Sum:	Sum Squared:	# Missing:
57.17	57.631	.461	1721.853	98826.511	0
Median:	Mode:	Kurtosis:	Skewness:		
57.391	•	-1.203	.024		

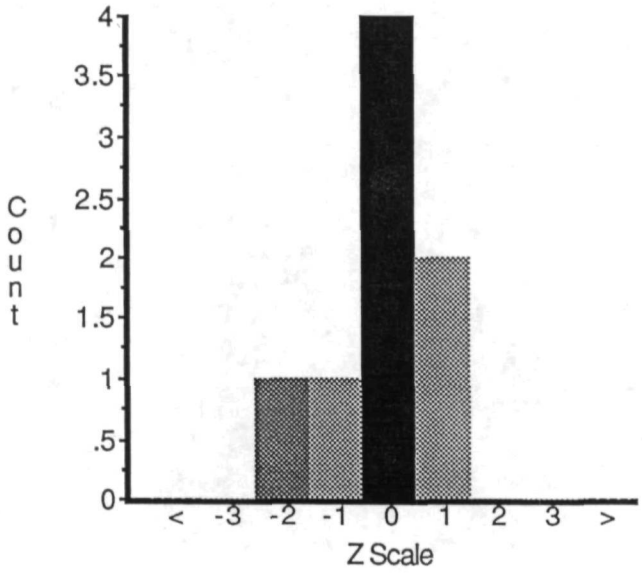
Z Score of AREA VIA BOTTOM ELEVATIONS



AREA VIA BOTTOM ELEVATIONS

Mean:	Std. Dev.:	Std. Error:	Variance:	Coef. Var.:	Count:
57.285	.205	.072	.042	.358	8
Minimum:	Maximum:	Range:	Sum:	Sum Squared:	# Missing:
57.071	57.615	.544	458.283	26253.207	0
Median:	Mode:	Kurtosis:	Skewness:		
57.245	•	-1.301	.367		

Z Score of AREA V BOTTOM ELEVATIONS

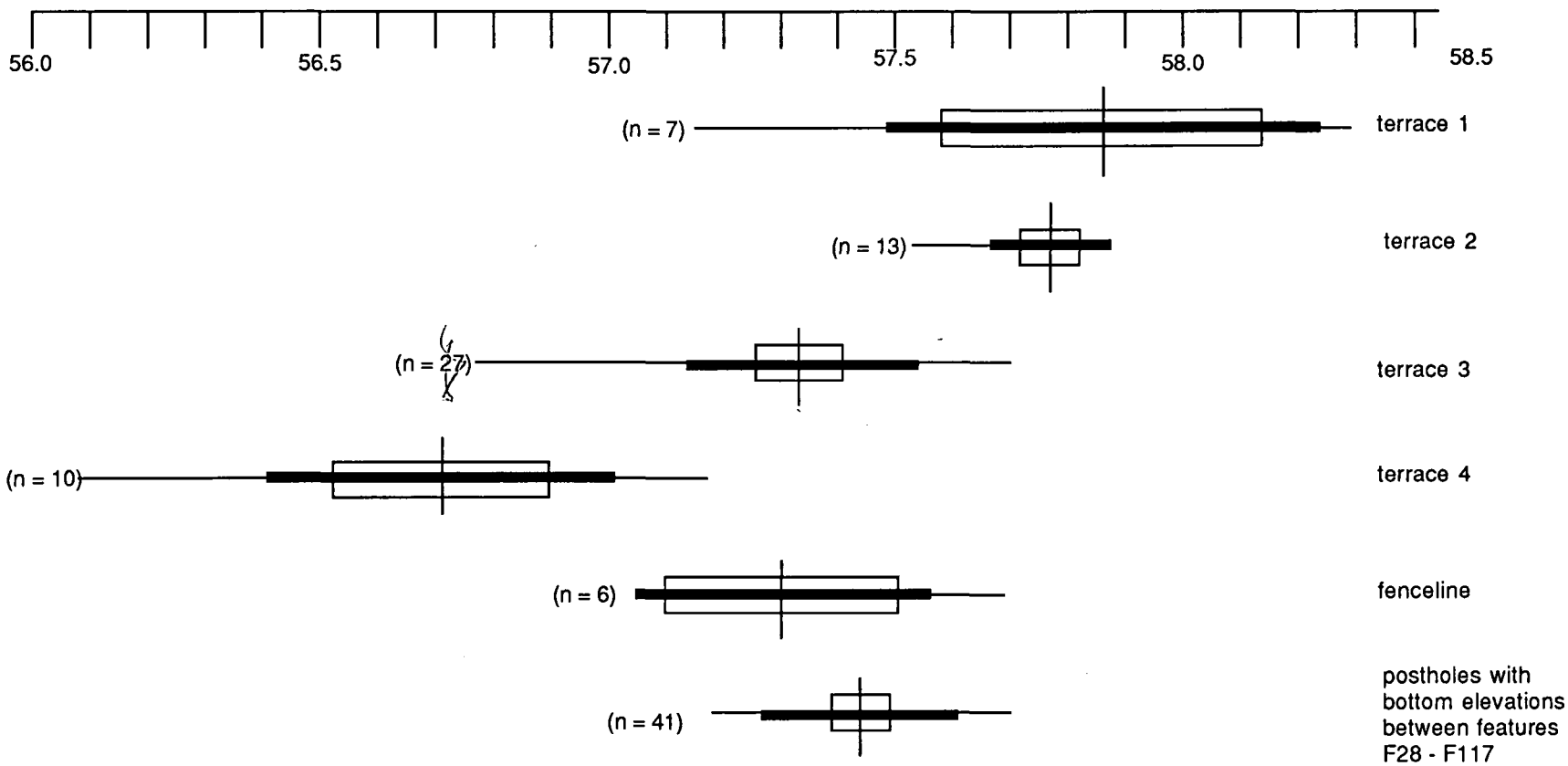


AREA V BOTTOM ELEVATIONS

Mean:	Std. Dev.:	Std. Error:	Variance:	Coef. Var.:	Count:
58.602	.051	.018	.003	.087	8
Minimum:	Maximum:	Range:	Sum:	Sum Squared:	# Missing:
58.52	58.674	.154	468.813	27473.222	0
Median:	Mode:	Kurtosis:	Skewness:		
58.611	•	-.918	-.305		

249	57.177	57.217	.040	4	•	•	•	##	•	•	•
20	57.618	57.698	.080	3	•	•	##	•	•	•	##
162	57.431	57.511	.080	3	•	•	##	•	•	•	##
48	56.718	56.818	.100	4	•	•	•	##	•	•	•
268	57.261	57.381	.120	3	•	•	##	•	•	•	##
160	57.702	57.832	.130	3	•	•	##	•	•	•	##
266	57.451	57.611	.160	3	•	•	##	•	•	•	##
222	57.511	57.682	.171	3	•	•	##	•	•	•	##
19	57.400	57.584	.184	3	•	•	##	•	•	•	##
22	57.582	57.774	.192	3	•	•	##	•	•	•	##
45	57.588	57.788	.200	3	•	•	##	•	•	•	##
125	57.047	57.247	.200	4	•	•	•	##	•	•	•
220	57.718	57.923	.205	2	•	57.718	•	•	•	##	•
237	57.962	58.172	.210	1	##	•	•	•	##	•	•
239	56.805	57.025	.220	4	•	•	•	##	•	•	•
50	57.842	58.062	.220	2	•	57.842	•	•	•	##	•
26	57.272	57.492	.220	3	•	•	##	•	•	•	##
267	57.311	57.531	.220	3	•	•	##	•	•	•	##
242	57.692	57.912	.220	2	•	57.692	•	•	•	##	•
136	57.682	57.912	.230	2	•	57.682	•	•	•	##	•
96	57.649	57.881	.232	2	•	57.649	•	•	•	##	•
14	57.952	58.192	.240	1	##	•	•	•	##	•	•
73	57.491	57.741	.250	3	•	•	##	•	•	•	##
208	57.764	58.052	.263	2	•	57.764	•	•	•	##	•
164	57.326	57.591	.265	3	•	•	##	•	•	•	##
218	58.292	58.562	.270	1	##	•	•	•	##	•	•
92	57.369	57.642	.273	3	•	•	##	•	•	•	##
25	57.448	57.728	.280	3	•	•	##	•	•	•	##
90	57.345	57.625	.280	3	•	•	##	•	•	•	##
247	57.306	57.616	.310	3	•	•	##	•	•	•	##
241	57.552	57.872	.320	2	•	57.552	•	•	•	##	•
182	58.147	58.467	.320	1	##	•	•	•	##	•	•
207	56.807	57.132	.325	4	•	•	•	##	•	•	•
129	57.632	57.962	.330	2	•	57.632	•	•	•	##	•
18	57.062	57.397	.335	3	•	•	##	•	•	•	##
244	57.296	57.636	.340	3	•	•	##	•	•	•	##
3	57.514	57.854	.340	2	•	57.514	•	•	•	##	•
95	57.631	57.981	.350	2	•	57.631	•	•	•	##	•
30	57.193	57.552	.359	3	•	•	##	•	•	•	##
221	57.440	57.800	.360	3	•	•	##	•	•	•	##

BOTTOM ELEVATIONS OF STRUCTURAL POSTHOLES

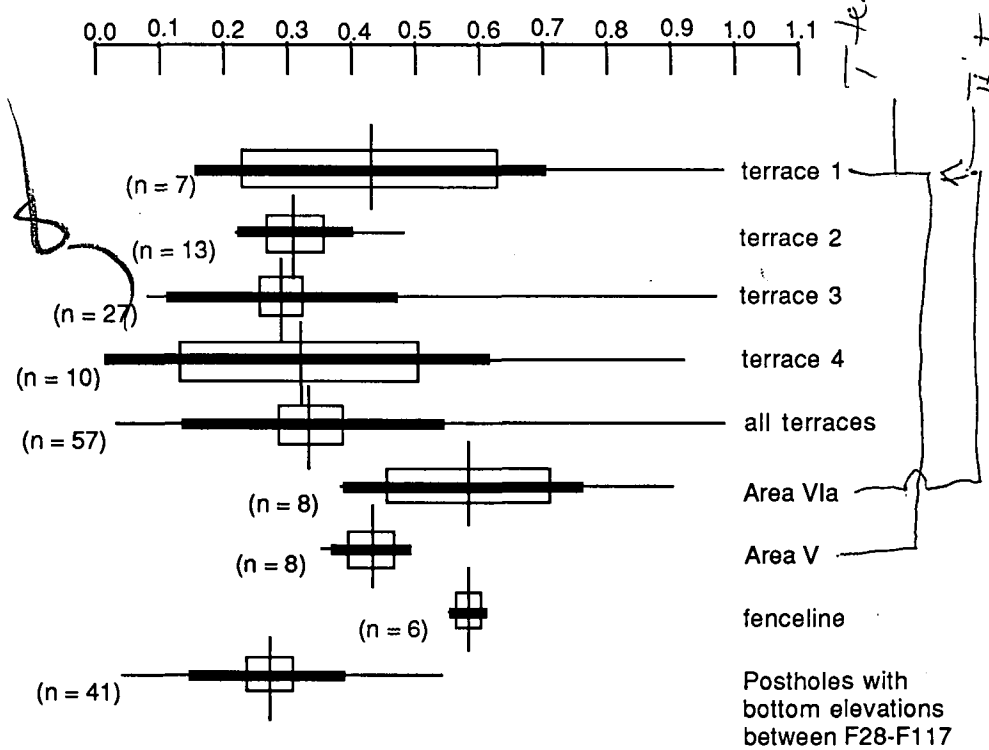


Mean value

Range of 2 standard errors around mean

Range of 1 standard deviation around mean

Range of observed values



Mean value

Range of 2 standard errors around mean

Range of 1 standard deviation around mean

Range of observed values

unpaired
DF = 13 1
mean .429
t = -.019
P > .40
LF no difference

V
.431

T test

Test
unpaired
DF 13
$\bar{x}$ .429 - .582
t = -1.316
.10 < p ≤ 3.75

terrace 1 & 2
1.603

unpaired test
.05 < p ≤ .10

terrace 1 & 3

Feature -	Westside	Bottom
128	1.1550	1.375

CONTOUR MAP - 10 cm INTERVAL ON MAP.

REDRAW HURRY'S MAP.

___ SHOOT FROM S 220 E 230 - H.I. - 1.47

___ BACK SHOOT TO S 200 E 230 - ELEVATION

___ SHOOT S200 E 200 → ELEVATION - H.I. + 4 8 m = ELEVATION OF S 220 E 230 ASL.

HURRYS MAP WAS DRAWN ON A 50 cm CONTOUR INTERVAL

	RAW ELEV	MINUS H.I.	(+ 48 m) ABOVE S200E200
S 200 E 200	3 m +		
S 200 E 230	2.773		
S 210 E 250	1.148		
S 220 E 210	2.618		

___ SHOOT SOUTH OF TRANSIT ALONG E 230 LINE

___ SHOOT NORTH ALONG E230 BAULK LINE TO S200 E230 AT 10 cm INTERVALS.

SHOOT ALONG E 220 BAULK

SHOOT ALONG E210 LINE

SHOOT ALONG S 210 LINE

BRICK RUBBLE

S 222 E 230 - BASE OF RUBBLE PILE 1.232

S 222 E 228 - 1.368

S 222 E 226 - 1.350

S 222 E 224 - 1.352

S 222 E 222 - 1.699

S 222 E 220 - 1.847

S 222 E 218 - 2.067

S 222 E 216 - 2.155

S 222 E 214 - 2.270

S 222 E 212 - 2.405

S 220 E 231 - 1.387

S 220 E 232 - 1.126 (BRICK RUBBLE)

S 220 E 233 - .765

S 220 E 234 - .258

S 220 E 235 - .082

S 220 E 236 - .156

S 220 E 237 - .553

S 220 E 238 - .861

S 220 E 239 - .1875

S 220 E 240 - 1.068

S 218 E 234 - 1.17

S 216 E 234 - 1.489

S 216 E 232 - 1.445

S 213 E 230 - 1.752

S 216 E 238 - 1.407

S 216.5 E 235 - 1.40

S 224 E 216 -

S 224 E 226 - .845

S 223 E 228 - 1.298

S 224 E 228 - .953

S 226 E 226 - .909

S 225 E 226 - .727

S 225 E 228 - .608

S 226 E 228 - .409

S 225.70 ~~S 226~~ E 230 - .003

(Beam & ARCH - INCLINATION FROM HORIZONTAL & DISTANCE)

S 224.70 E 230 - .170

S 223.70 E 230 - .512

S 222.70 E 230 - .886

S 224 E 222 - 1.30

S 224 E 220 - 1.378

S 224 E 218 - 1.472

S 224 E 216 - 1.541

S 224 E 214 - 1.736

S 224 E 212 - 1.780

S 226 E 222 - .975

S 226 E 220 ———

S 226 E 218 - 1.145

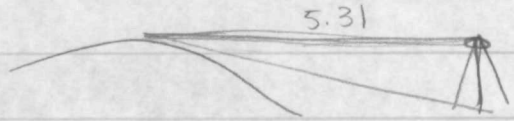
E 216 - 1.195

E 214 - 1.243

E 212 - 1.30

TOP OF RUBBLE

5.31



SCOPE ≮ 1½°

#1 1.435

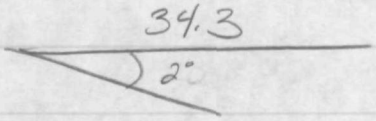
.397 = 1.038

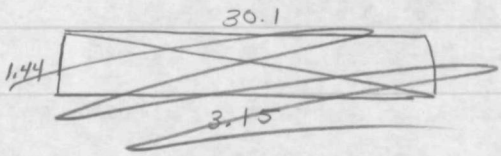
43.6

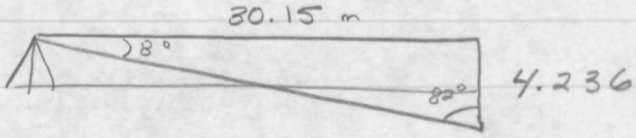
.3640

.0349

1.197 + 3







30.15 m

TAN 8° = .1405 2.796

a = b tan A

IF S200 E200 IS 2.796 m below S230 E203

THEN IF 200/200 = 0 230/203 IS 2.796 ABOVE

THIS. THEN

Julie,

as I told you, when I started the nail read 1.74.

I "redid" the features and the results are:
(the #'s of the first reading are in [ ]'s)

Feature	west side nail	east shelf	bottom
101	1.118 [1.20]		1.275
★ 117	.422 [.42]	.655 [.64]	.959 [.94]
4	.505 [.51]		.650
208	.625		.888 [.89]

★ Feature 117 is the monster of Daniel M's. The east shelf and bottom elevation numbers are so different because Robin wasn't able to return this rod to exactly the same place.

Now, when I reshot the nail, the crosshairs were not exactly on the nail. It looked to be about 1.73 (guesstamation)